

Effect of different types of electrospun polyamide 6 nanofibres on the mechanical properties of a carbon fibre/epoxy composites

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Research Alliance

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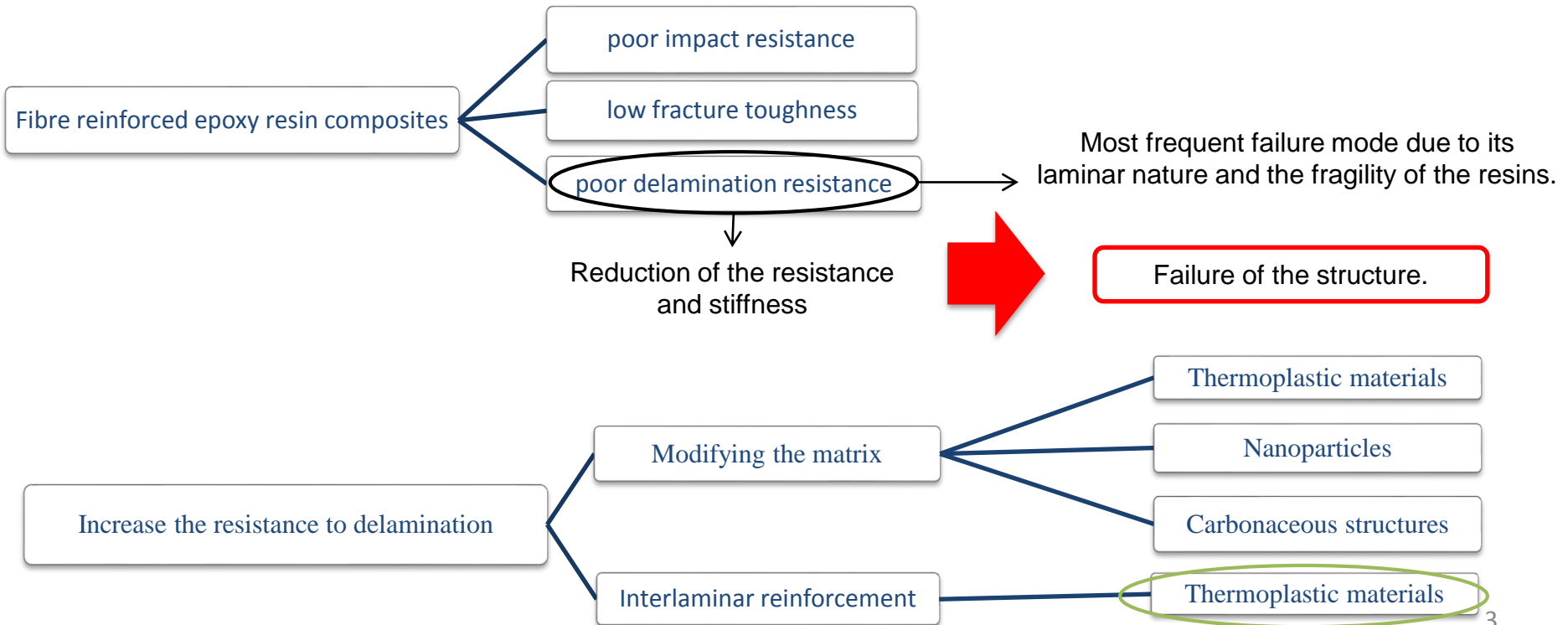
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1. INTRODUCTION

- Fibre reinforced epoxy resin composites are widely used in industry, owing to their high strength and stiffness at low weight, and their good corrosion-resistance and fatigue properties.



1. INTRODUCTION

Electrospun thermoplastic nanofibres veils

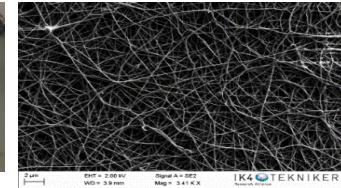
Properties

- Great surface/volume ratio
- High porosity
- Low area density
- Adjustable pore size
- Nanoscale fiber diameter
- High mechanical resistance
- High permeability

Advantages

Promising technique to toughen laminated composites without deteriorating the mechanical properties

- ✓ Thin veils → Their presence do not affect the thickness and weight.
- ✓ No need to disperse → No viscosity increase or a non-homogeneous dispersion
- ✓ High porosity → not impede the flow of resin



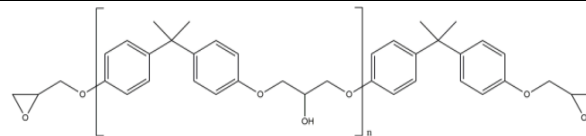
2. OBJECTIVE

The present work studies the effect of the incorporation of electrospun polyamide 6 nanofibre veils coming from two different type of pellets, in the final mechanical properties of carbon fibre epoxy composites with the objective to study the influence of the PA6 mechanical properties and nature in composite material.

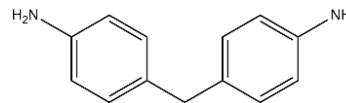
3. EXPERIMENTAL PART

Materials

Matrix_Diglycidyl ether of bisphenol A (DGEBA)



Curing agent_4,4'-diaminodiphenylmethane (DDM)



Carbon fibre fabric HT3k



PA6 Ultramid B24 N 03

Textile sector

PA6 Badamid B70

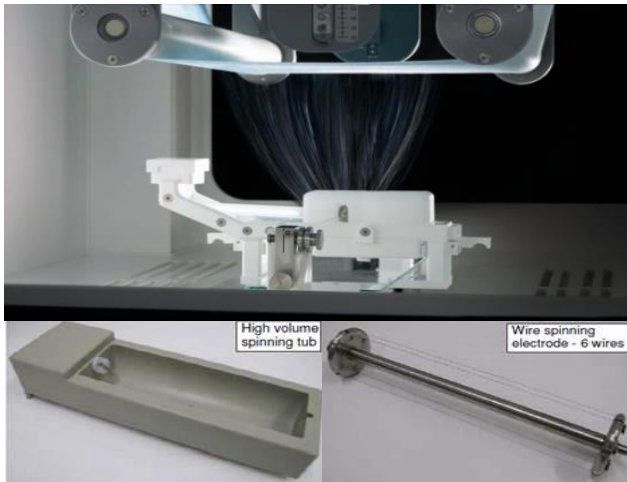
Industrial sector



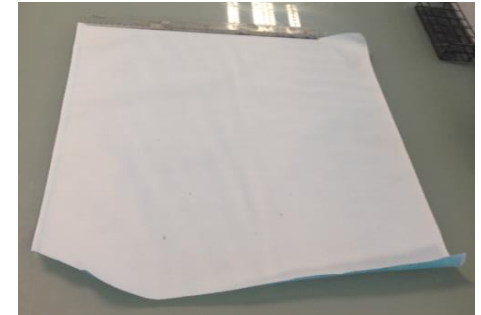
PA6 nanofibre veils preparation

3. EXPERIMENTAL PART

- 12 wt% of both types of PA 6 pellets were dissolved in the mixture 2:1 acetic acid:formic acid by stirring during 2 hours at 80°C.
- The nanofibres were produced using a multijet electrospinning setup Nanospider™, using a high volume spinning tub.
- The solution is poured into the feed unit and a cylindrical electrode formed by six wires is placed in the middle of the solution tank. The upward part has a second wire electrode, which has the opposite charge. The electrical field between the electrodes overcomes the surface tension of the polymer solution, forming thousands of jets that become fibres when the solvent is evaporated and they are deposited in the substrate.



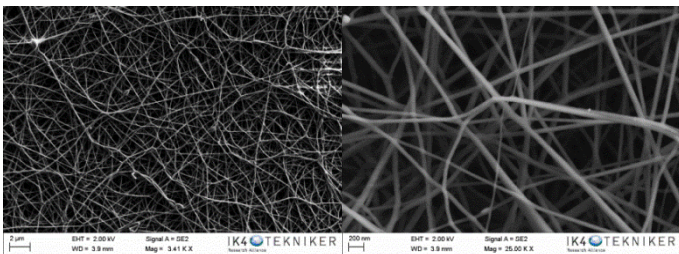
PA6 Badamid



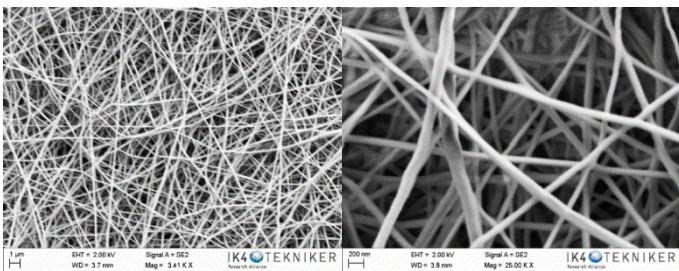
PA6 Ultramid

PA6 nanofibrous veils characterization

PA6
Ultramid



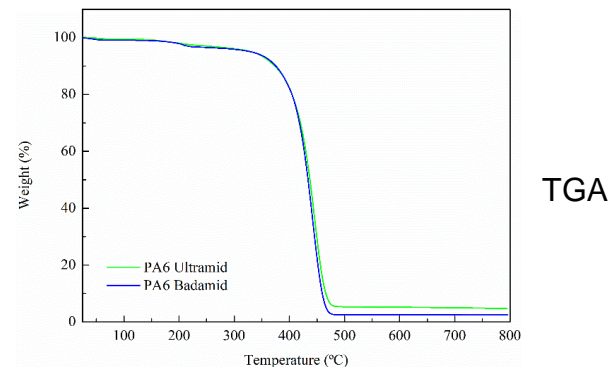
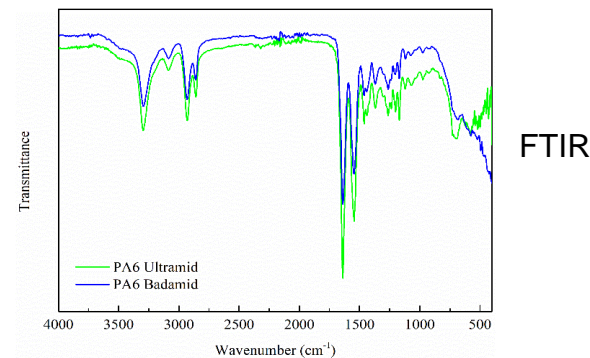
PA6
Badamid



continuous and
uniform nanofibre
network

System	Fibre diameter (nm)	Areal weight density (g/m ²)
PA6 Ultramid	60-100	1,94
PA6 Badamid	60-130	2,23

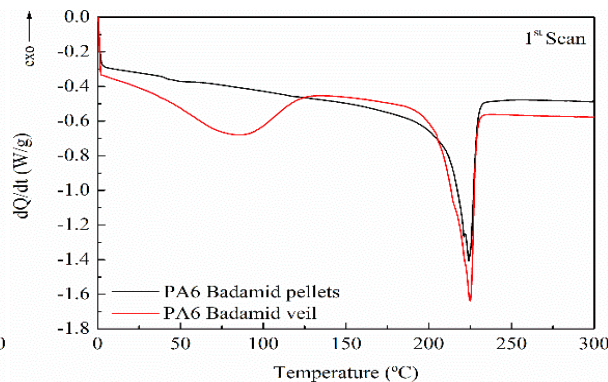
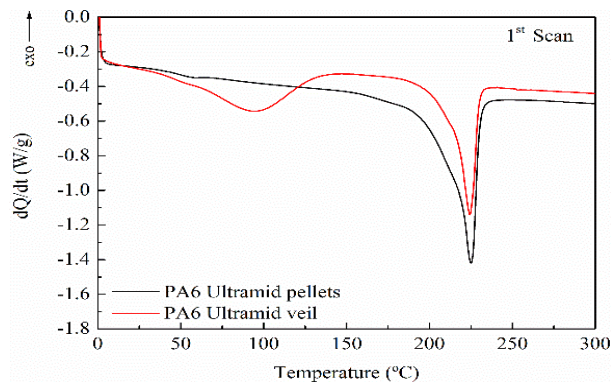
4. RESULTS AND DISCUSSION



No excess of solvent due to
the electrospinning process

PA6 nanofibrous veils characterization

4. RESULTS AND DISCUSSION



Thermal
characterization
(DSC)

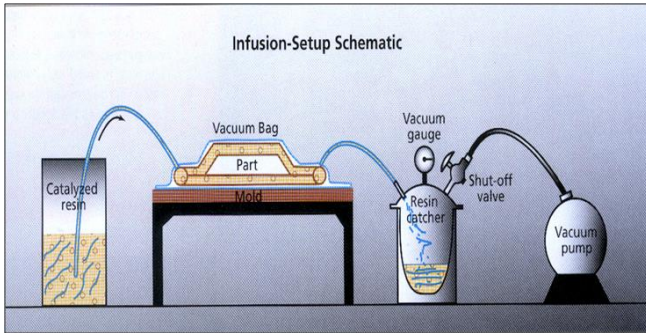
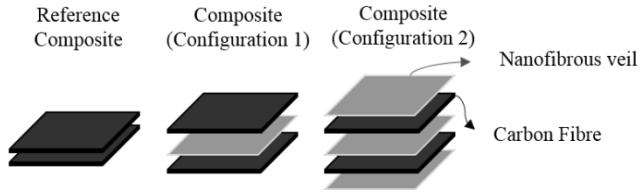
Material	T_f (°C)	ΔH_f (J/g)	X_c (%)
Ultramid pellets	225,1	107,1	46,5
Ultramid veil	224,3	61,2	26,6
Badamid pellets	224,1	95,4	41,5
Badamid veil	225,0	87,8	38,2

% Cristallinity pellets > Veils

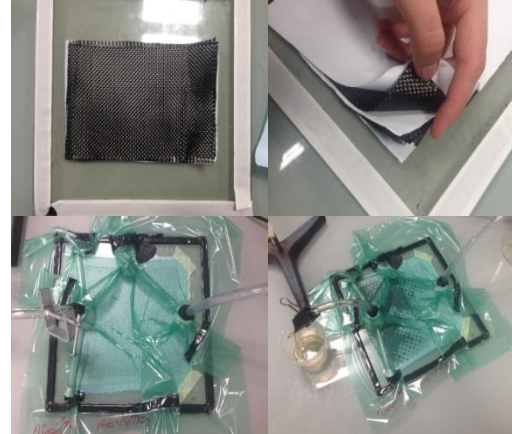
% Cristallinity PA6 Badamid > PA6 Ultramid

Composites manufacturing

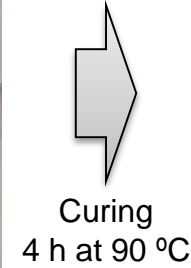
Two carbon fibre plies interleaved with stand-alone nanofibrous veils were prepared



3. EXPERIMENTAL SECTION



Infusion process



Curing
4 h at 90 °C



Reference
Composite
(thickness between
0.6-0.7 mm)

For the fracture test (mode I, mode II), composites with 14 layer of carbon fibre and an interlaminar veil in the central axis have been developed also using vacuum infusion technique.

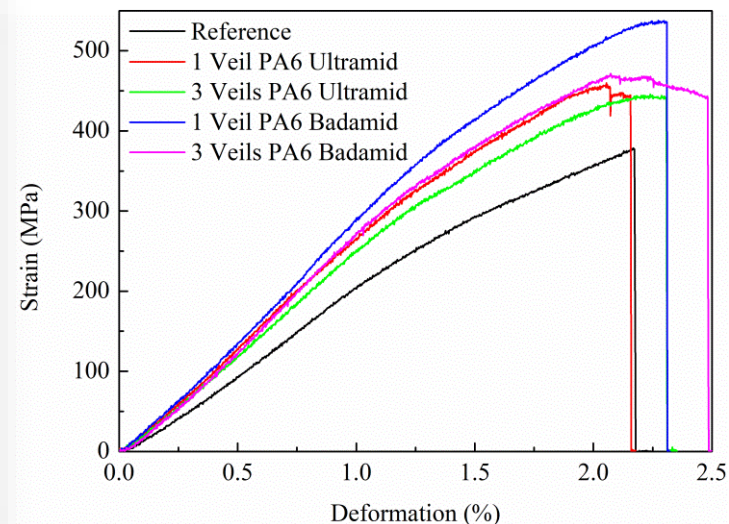
Composites characterization

Flexure test



Sample	σ_{max} (MPa)	$\Delta\sigma_{max}$ %	δ_{max} (%)
Reference	375.5±33.2		2.2±0.2
1 veil PA6 Ultramid	449.5±10.8	19.7	2.1±0.0
3 veil PA6 Ultramid	415.4±23.8	10.6	2.1±0.2
1 veil PA6 Badamid	534.6±28.9	42.4	2.3±0.0
3 veil PA6 Badamid	502.3±48.5	33.8	2.1±0.1

4. RESULTS AND DISCUSSION



Both, PA6 Ultramid and PA6 Badamid nanofibrous veils, toughen composite laminates considerably

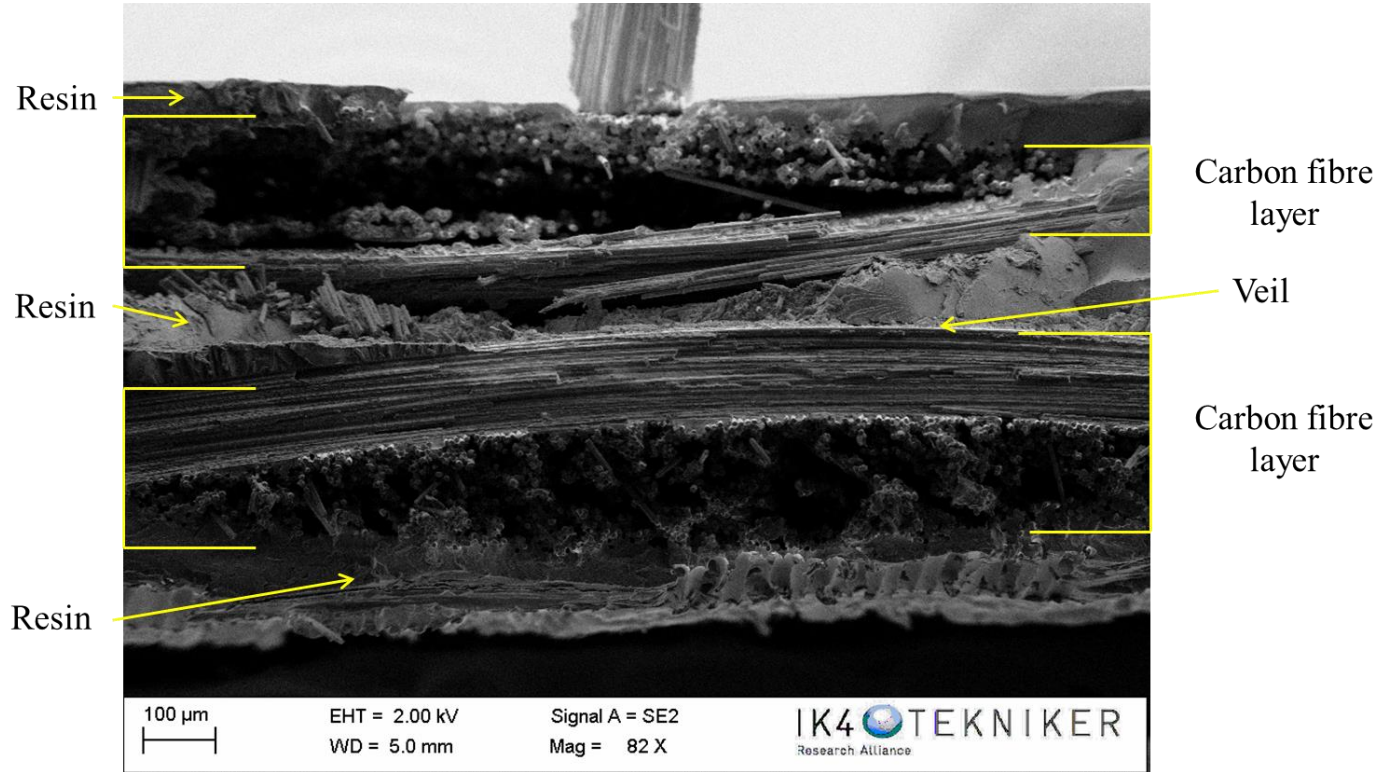
$$\sigma_{max} \text{ 1 Veil} > \sigma_{max} \text{ 3 Veils}$$

The outer veils do not contribute positively to the improvement flexural mechanical properties

Composites characterization

4. RESULTS AND DISCUSSION

Fractographic SEM analysis



1 Veil PA6 Ultramid

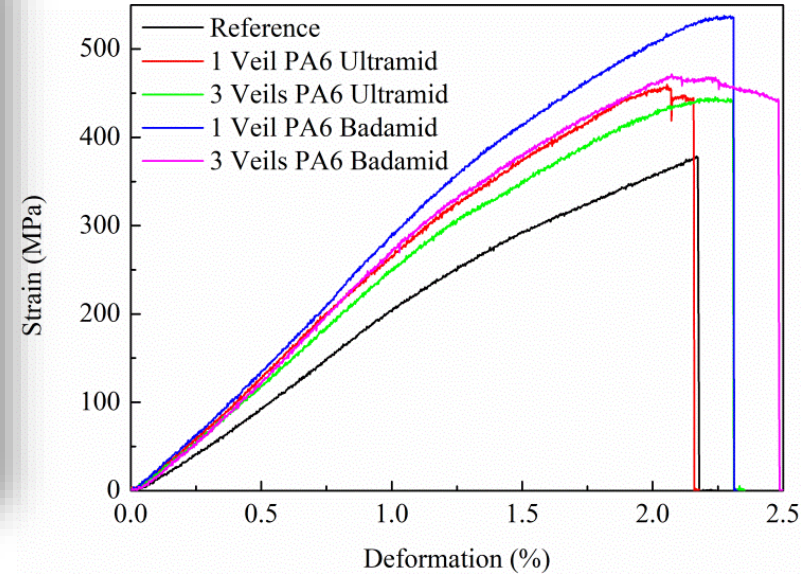
Composites characterization

Flexure test



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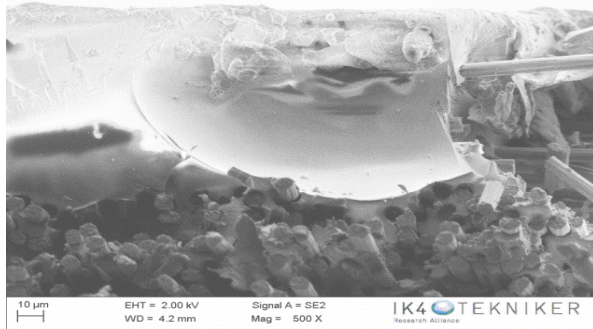
4. RESULTS AND DISCUSSION



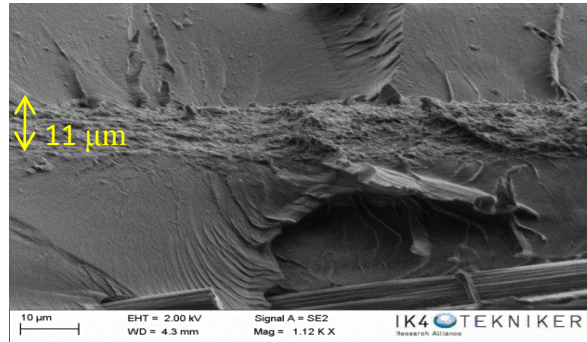
σ_{max} Badamid veil > σ_{max} Ultramid Veil

Composites characterization

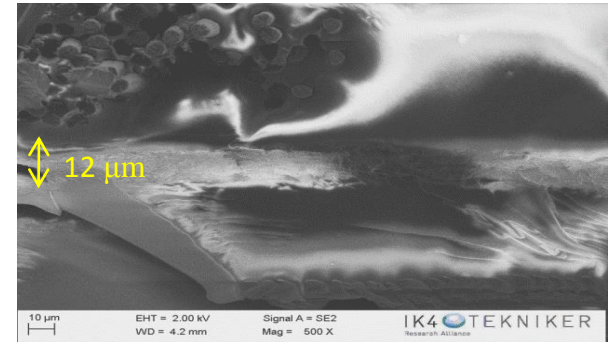
Fracture waves of the resin end in the veil
The veils prevent the propagation of the crack through the polymeric matrix



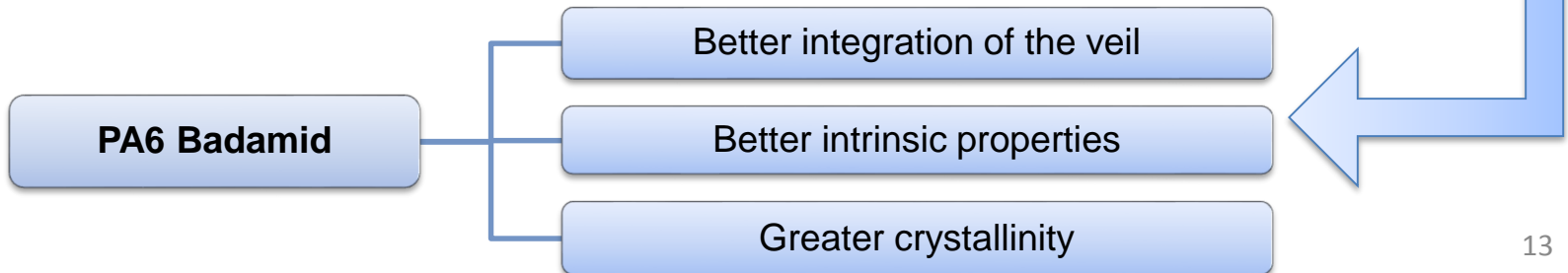
Reference



1 Veil PA6 Ultramid
Interlaminar Veil



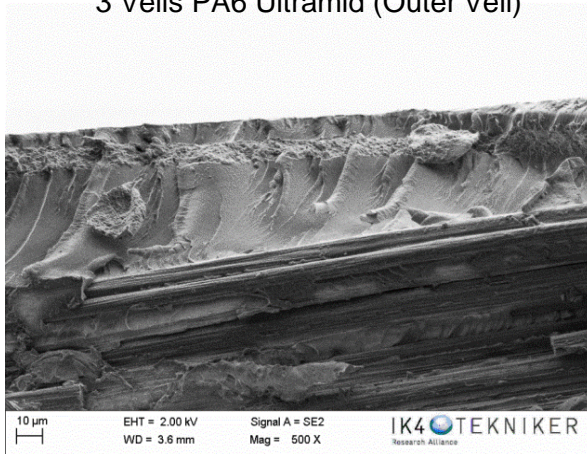
1 Veil PA6 Badamid
Interlaminar Veil



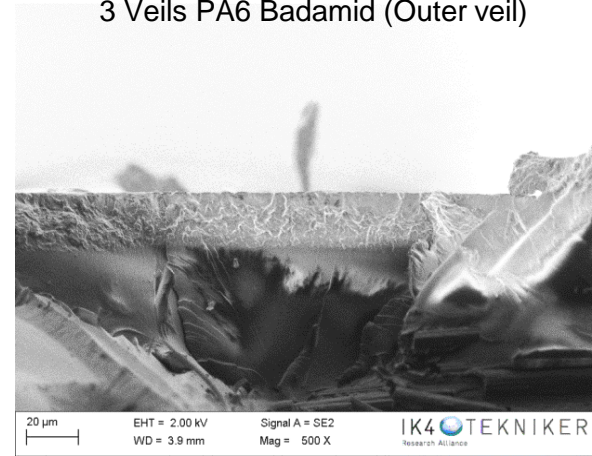
Composites characterization

While the interlaminar veil clearly stops the crack propagation, the outer veils do not seem to contribute to avoid it

3 Veils PA6 Ultramid (Outer Veil)



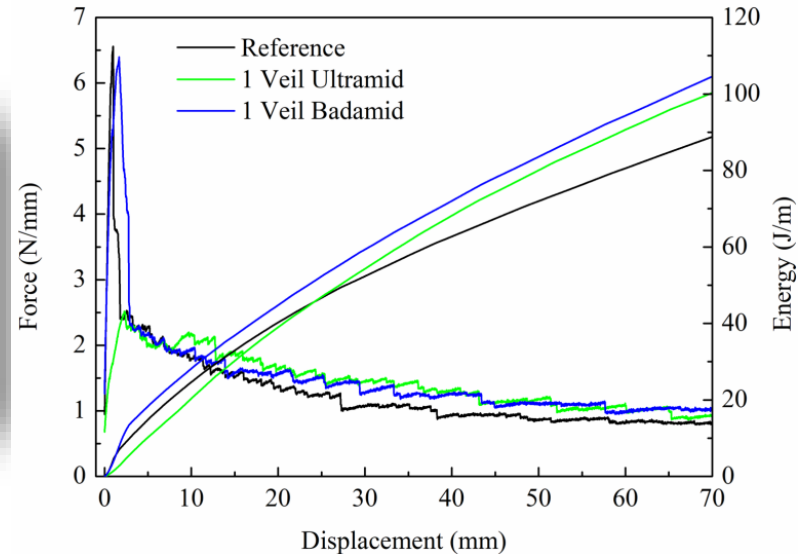
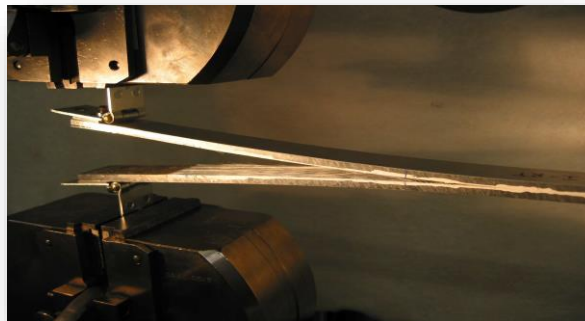
3 Veils PA6 Badamid (Outer veil)



- A difference in the position of the outerveils is appreciated
- The infusion process can result in composite materials with a very thin external face of resin or an outer face formed by the resin impregnated veil

Composites characterization

Fracture Mode I test

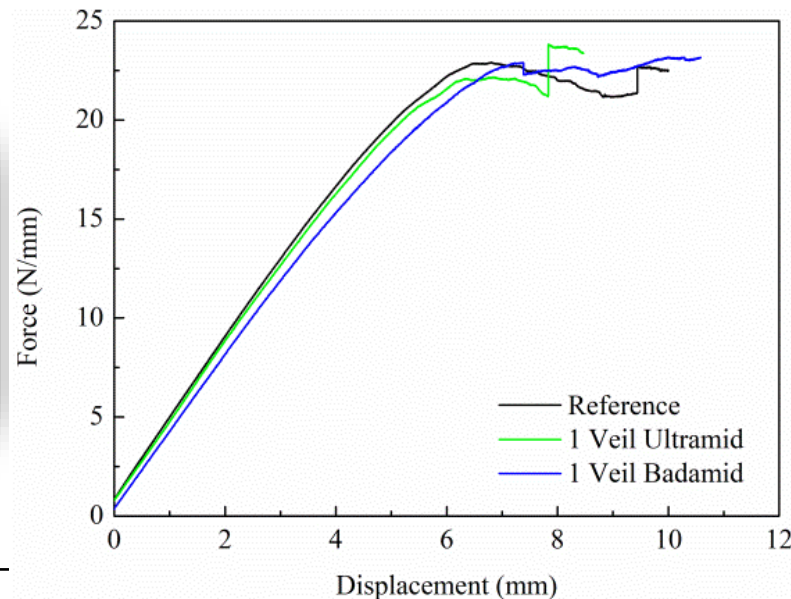
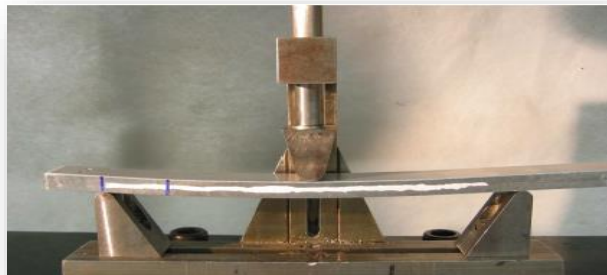


Sample	Load (N/mm)	$\Delta\%$	Energy (J/m)	$\Delta\%$	G_{IC} (J/m ²)	$\Delta\%$
Reference	6.6±0.8		62.7		389±12.8	
PA6 Ultramid	2.5±0.1	62.9	68.1	8.6	466±73.0	20.0
PA6 Badamid	6.4±0.1	2.6	72.0	14.8	560±72.3	44.0

The presence of the veil tends to impede the propagation of the crack

Composites characterization

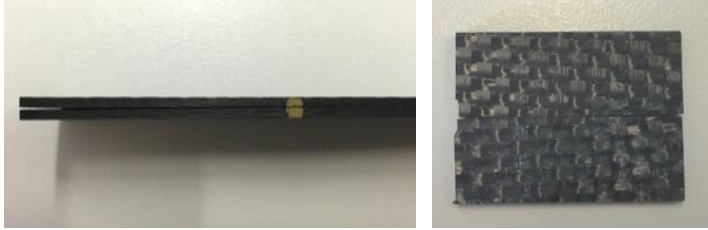
Fracture
Mode II test



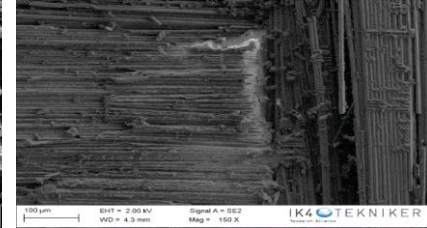
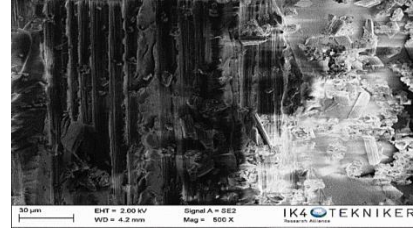
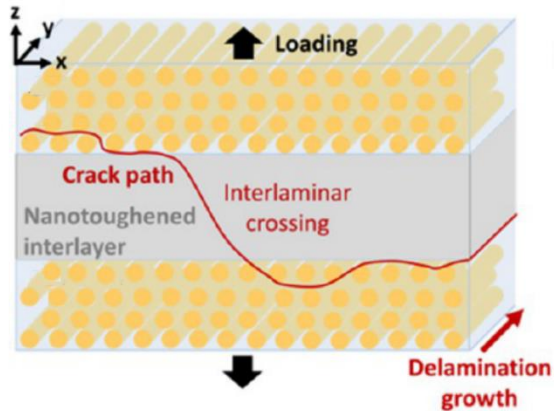
Sample	Load (N/mm)	$\Delta\%$	G_{IIC} (J/m ²)	$\Delta\%$
Reference	22.7±2.7		2536.8±257.7	
PA6 Ultramid	22.1±1.4	2.6	2544.0±304.0	0.3
PA6 Badamid	22.6±0.4	0.4	2970.9±526.0	16.8

The maximum load reached is similar
No significant improvement is reached

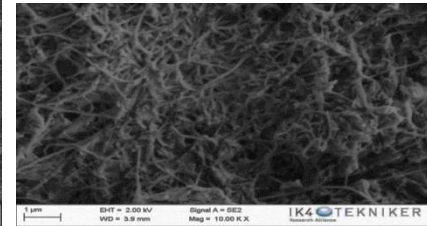
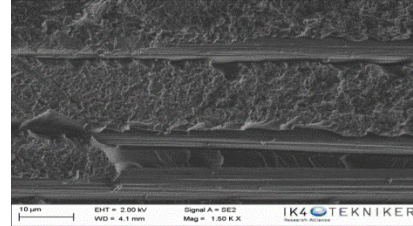
Composites characterization



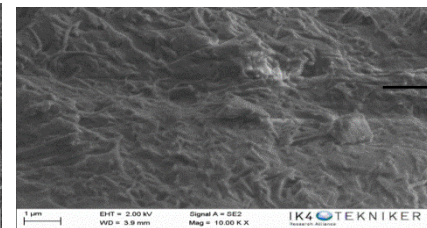
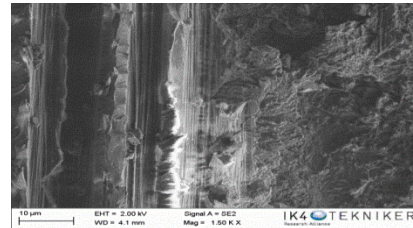
The surface of the veils remains in both sides of the composite specimen and the crack propagates partially between the carbon fibre and the veil



Reference



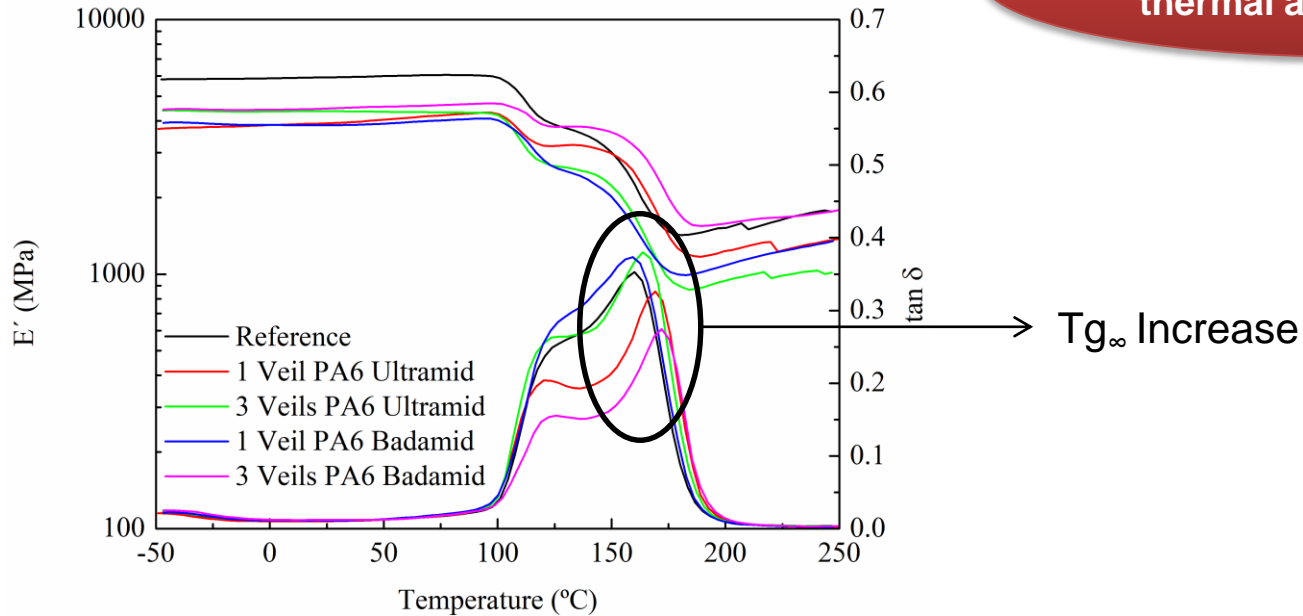
1 veil PA6 Ultramid



1 veil PA6 Badamid

→ more integrated in the resin

Composites characterization



Dynamic mechanical thermal analysis (DMTA)

5. CONCLUSIONS

- The incorporation of polyamide nanofibre veils increase their mechanical properties.
- For composites with one PA6 nanofibre veil between the carbon fibre plies, the stress at failure during the flexural mechanical tests increased 19.7% and 42.4 % for composites modified with PA6 Ultramid and PA6 Badamid, respectively.
- The analysis of the fractured surfaces, carried out by SEM, indicated that the veil hindered the crack propagation in the composites.
- The veils from Badamid, with higher crystallinity, conduct to better results than the veils from Ultramid.
- The fracture toughness analysis showed that G_{IC} value increased 20 and 44% for composites modified with a veil of PA6 Ultramid and PA6 Badamid, respectively, whereas G_{IIC} values only increase slightly for the composite modified with the veil of PA6 Badamid. This increment is due to the crack propagation across the PA6 veil, which result in a high energy absorption of the veil.

The inclusion of electrospun polyamide 6 nanofibre veils on the carbon fibre/epoxy composites resulted in a significant improvement in mechanical properties, both flexural and fracture toughness, without an increase in laminate thickness, weight and maintaining or slightly increasing the glass transition temperature of the composite.

ACKNOWLEDGMENTS

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THANK YOU FOR YOUR ATTENTION

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