

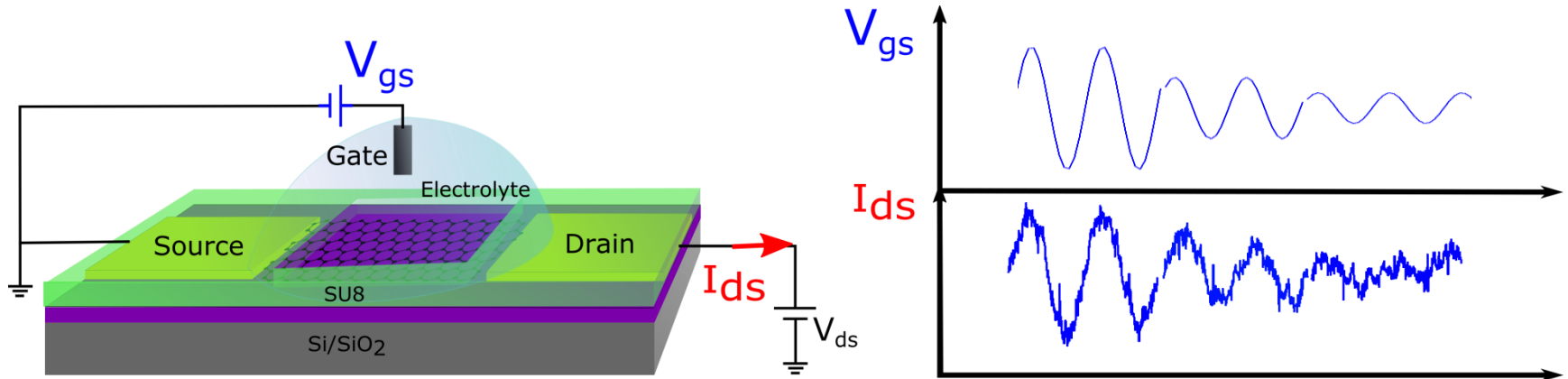


Low-Frequency Contact Noise mitigation in graphene-FETs

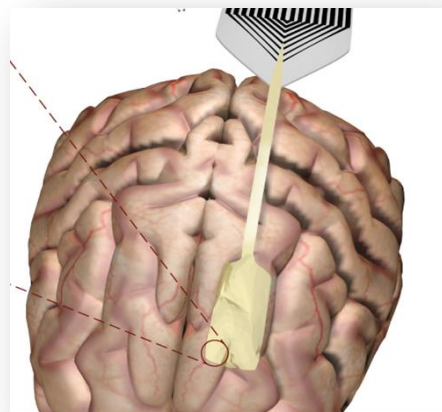
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Low-frequency noise (LFN) limits sensing applications of graphene

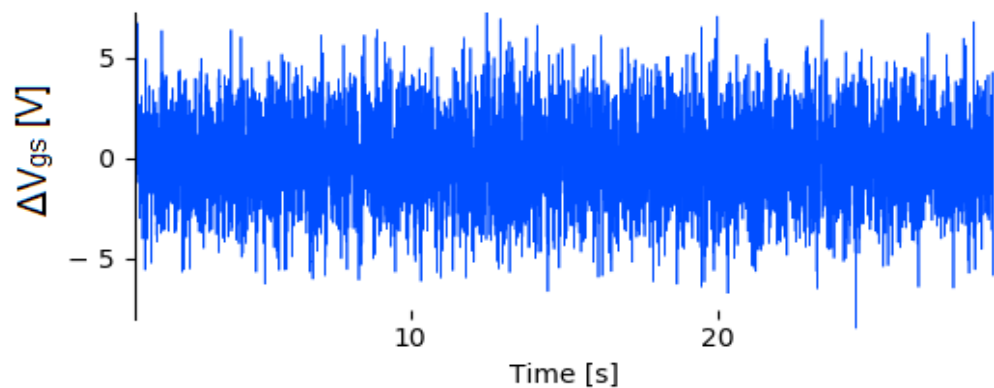


$$I_{ds} = G_m \underbrace{\Delta V_{gs}}_{\Delta V_{gs-signal} + \Delta V_{gs-noise}}$$

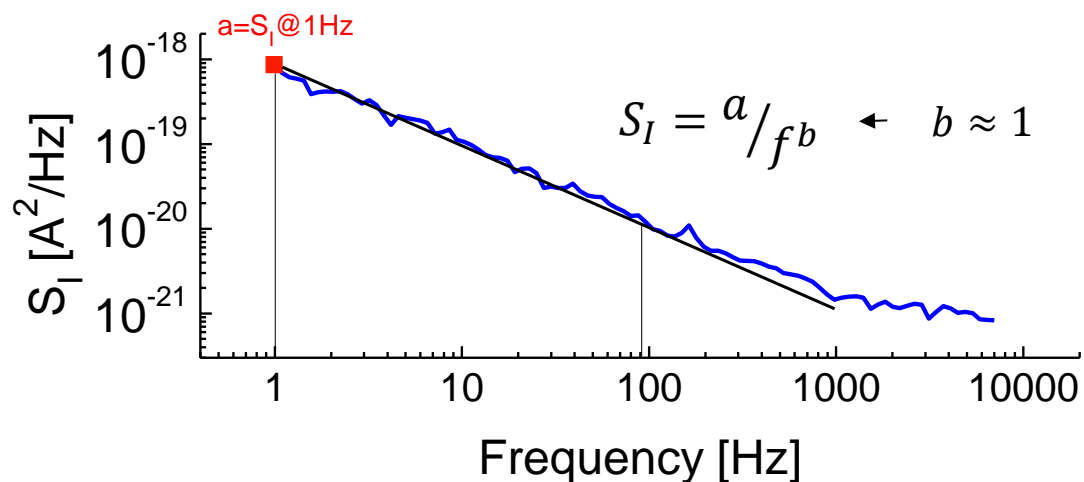


- Minimizing the noise level is crucial to maximize the sensitivity of the device

How is noise power measured?



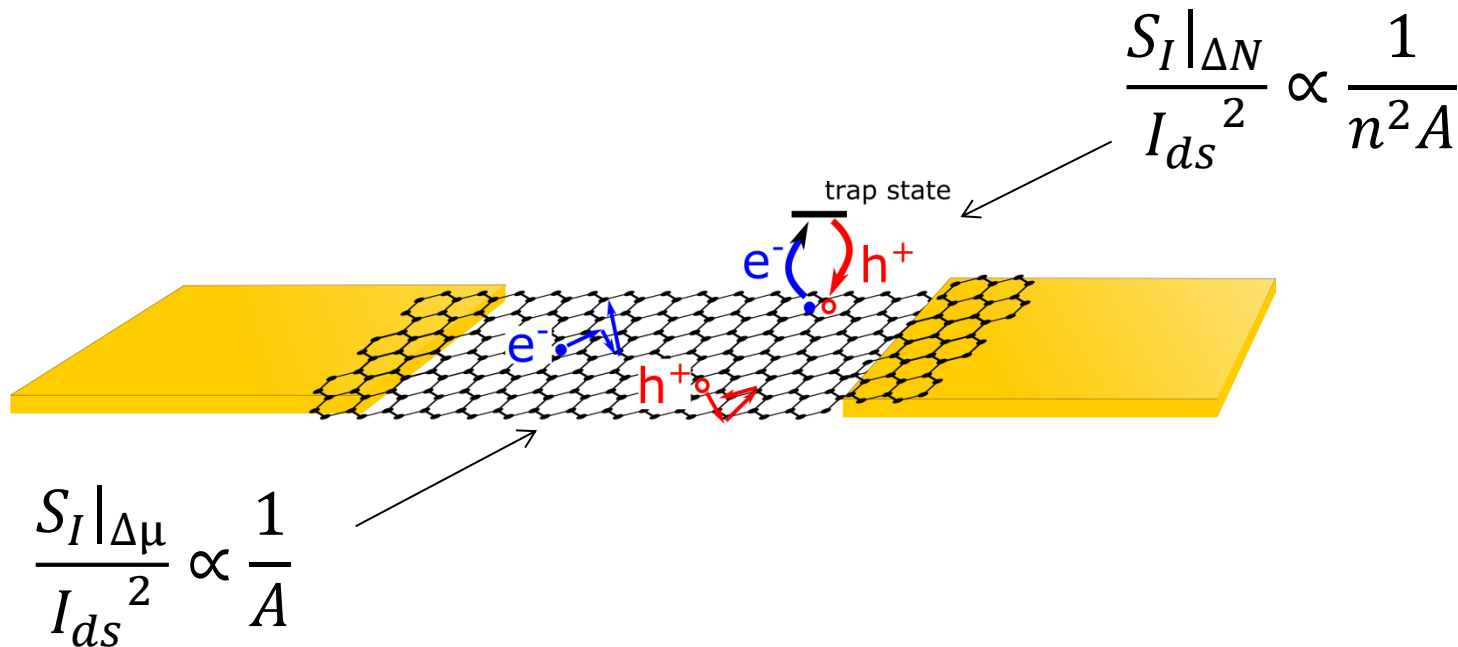
FFT



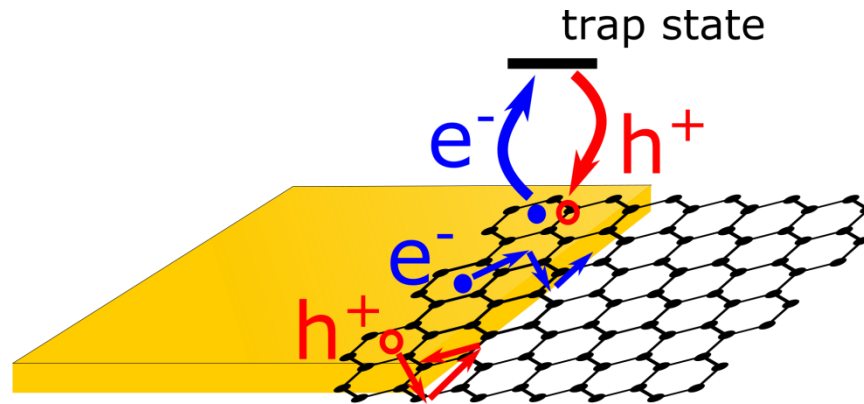
$$I_{ds-rms} = \sqrt{\int S_I df} \propto \sqrt{a}$$

What is the origin of noise?

- Charge trapping-detrapping noise
- Mobility fluctuation noise



Is noise generated at the contacts?




$$\frac{S_{R_c}}{R_c^2} \stackrel{?}{\propto} \frac{1}{A_c n^2}$$

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If current was injected mainly through the edge of graphene it'd be one or another

We want to
measure contact noise

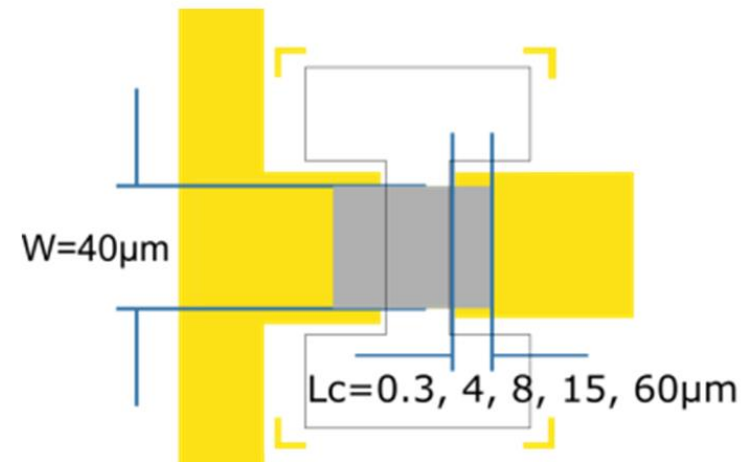
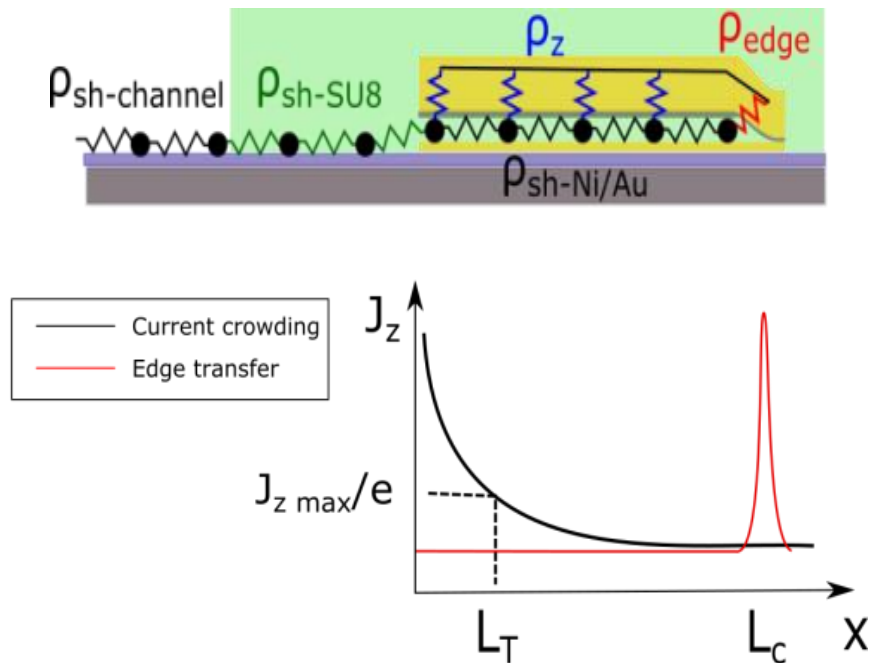
We want to **eliminate it**



What is the **geometric dependence** and **origin** of contact noise?

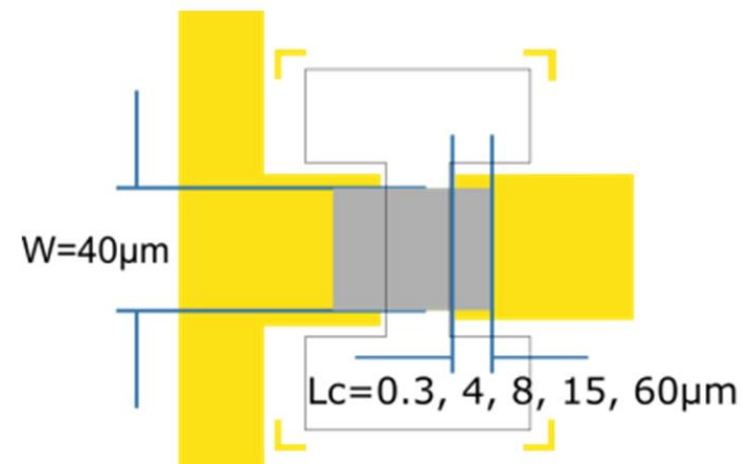
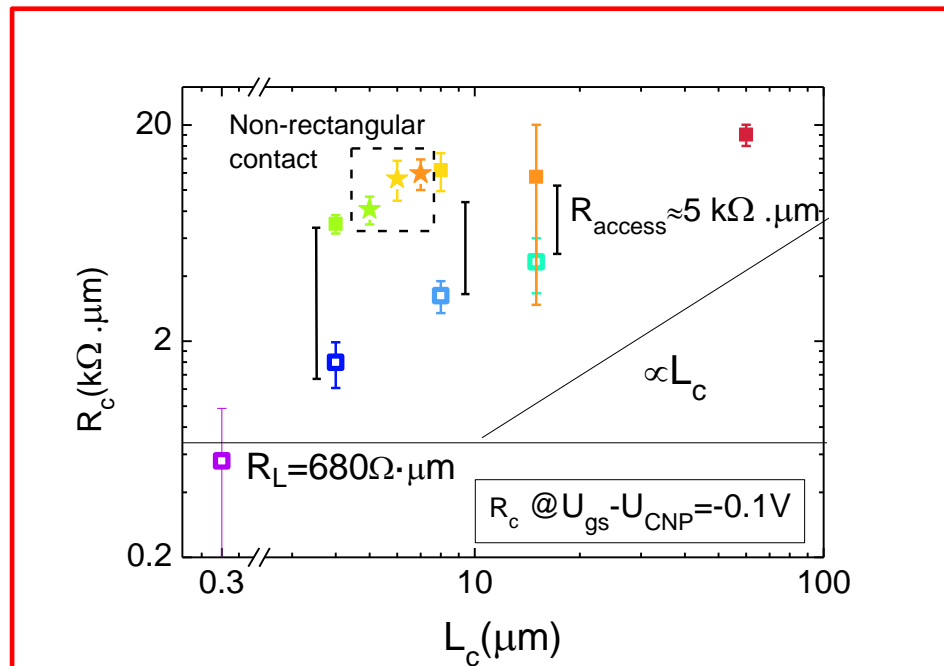
First, what is the **geometric dependence** of contact resistance?

- z-plane injection and edge injection have different geometry dependence



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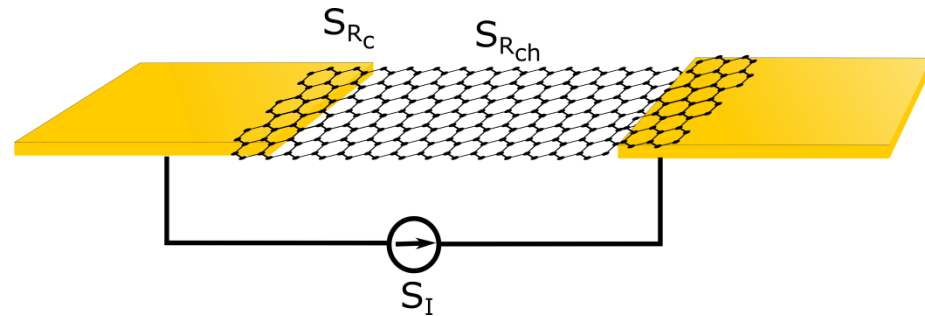


Injection through the edges dominates!

Then, what is the **geometric dependence** and **origin** of contact noise?

- Take the general equation:

$$\frac{S_I}{I_{ds}^2} = \frac{S_{R_c} + S_{R_{ch}}}{R_T^2}$$



- If charge trapping-detrapping dominates:

$$\frac{S_I}{I_{ds}^4} = \frac{k}{A_c n_c^2 V_{ds}^2} R_c^2 + \frac{k}{A_{ch} n_{ch}^2 V_{ds}^2} R_{ch}^2$$

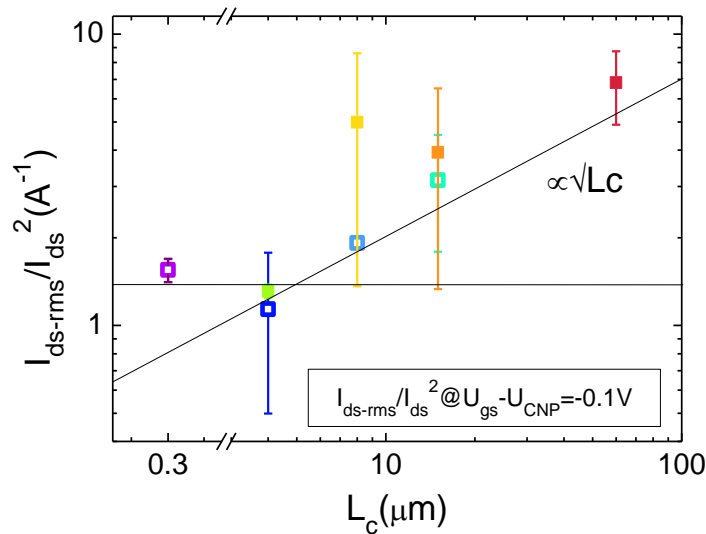
- If contacts contribution dominates:

$$\frac{S_I}{I_{ds}^4} \propto L_c \quad \text{geometry}$$

$$\frac{S_I}{I_{ds}^4} \propto R_c^4 \quad \text{origin}$$

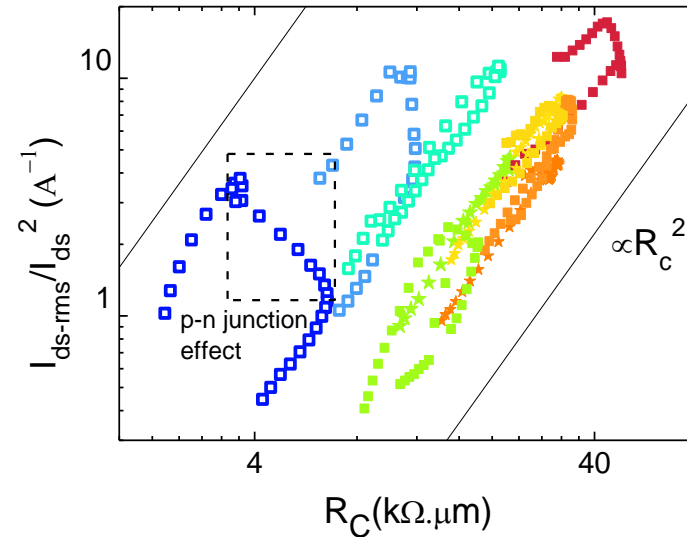
Geometry and origin of contact noise:

$$\frac{I_{rms}}{I_{ds}^2} \propto \sqrt{L_c}$$



Noise increases with L_c

$$\frac{I_{rms}}{I_{ds}^2} \propto R_c^2$$



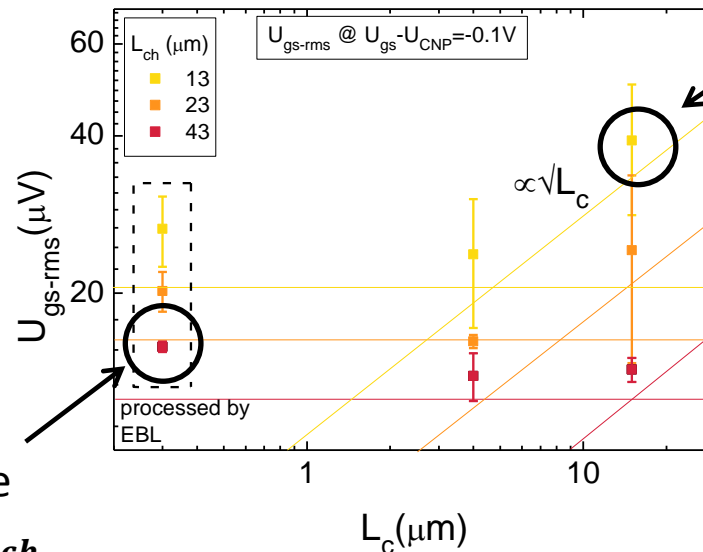
Charge trapping-detrapping noise

Can contact noise be measured and reduced by geometric design?

- From the general noise equation:

$$\frac{S_I}{I_{ds}^4} = \frac{kL_c}{V_{ds}^2 W^3} + \frac{kL_{ch}}{V_{ds}^2 W^3}$$

Contact noise can be measured if $L_c \gg L_{ch}$



Contact noise can be minimized if $L_c \ll L_{ch}$

To summarize

- There is a contribution from contacts to noise
- The geometric dependence of the contact resistance and noise can be determined by changing L_C
- The relative importance of the contacts contribution to noise can be changed by design

